

Isolated DC/DC Converter IC

Isolated Type Fly-back Converter IC with Integrated Switching MOSFET for Automotive

BD7F105EFJ-C

General Description

BD7F105EFJ-C is an opto-coupler-less isolated flyback converter. Feedback circuit by optocouplers or the auxiliary winding of transformers becomes unnecessary, contributing to reduction of set parts. Furthermore, the adoption of original adapted ON-time control technology enables fast load response. In addition, the various protection function realizes the designs of isolated power supply application for high reliability.

Features

- AEC-Q100 Qualified^(Note 1)
- No Need for Optocoupler and Third Winding of Transformer
- Set Output Voltage with Two External Resistors and Ratio of Transformer Turns
- Adopt of Original Adapted ON-time Control Technology Fast Load Response
- High Efficiency at Light Load Mode (PFM Operation)
- Shutdown Function / Enable Control
- Built-in 60 V Switching MOSFET
- Frequency Spectrum Spread
- Soft Start Function
- Load Compensation Function
- Various Protection Function
- Input Low Voltage Lockout (UVLO) Over Current Protection (OCP) Thermal Shutdown (TSD)
 REF Pin Open Protection (REFOPEN) Short Circuit Protection (SCP)
 Battery Short Protection (BSP)
 HTSOP-J8 Package
- (Note 1) Grade 1

Typical Application Circuit

Key Specifications

Input Voltage Range:	
VIN Pin	3.4 V to 42.0 V
SW Pin	60 V (Max)
Switching Frequency:	363 kHz (Typ)
Reference Voltage Precision:	± 2.8 % (Typ)
Shutdown Current:	0 µA (Typ)

Operating Ambient Temperature Range -40 °C to +125 °C

Package

HTSOP-J8

W (Typ) x D (Typ) x H (Max) 4.9 mm x 6.0 mm x 1.0 mm



Applications

- Automotive Isolated Power Supplies (E-Comp, Inverter etc)
 - Industrial Isolated Power Supplies



OProduct structure : Silicon integrated circuit OThis product has no designed protection against radioactive rays.

Contents

General Description	1
Features	1
Key Specifications	1
Package	1
Applications	1
Typical Application Circuit	1
Contents	2
Pin Configuration	3
Pin Descriptions	3
Block Diagram	3
Description of Blocks	4
 INTERNAL REGULATOR	4 5 5 5 5
 8 Maximum Frequency Limit Function (MAX FREQ) 9 DRIVER 	5 5
 Nch MOSFET LOAD COMPENSATION	6 6 6
14 Short Circuit Protection (SCP), REF Pin Open Protection (REFOPEN) Absolute Maximum Ratings	8
Thermal Resistance	8
Recommended Operating Conditions	8
Electrical Characteristics	9
Typical Performance Curves	10
Application Examples	18
 Output Voltage	20 22 22 23
 7 Snubber Circuit 8 Setting of SDX/EN Pin Resistor 9 The Output Voltage Compensation Function by L_COMP Pin Resistor 10 The Influence to Frequency and Output Voltage for Each Load I/O Equivalence Circuits 	24 25 26
Operational Notes	28
Ordering Information	30
Marking Diagram	30
Physical Dimension and Packing Information	31
Revision History	32

Pin Configuration



Pin Descriptions

Pin No.	Pin Name	Function			
1	GND	GND pin			
2	SDX/EN	Shutdown/Enable control pin			
3	L_COMP	Setting pin of load current compensation value pin			
4	REF	Output voltage setting pin			
5	FB	Output voltage setting pin			
6	N.C.	No Connect ^(Note 1)			
7	SW	Switching output pin			
8	VIN	Power supply input pin			
-	EXP-PAD	Connect EXP-PAD to GND on PCB ^(Note 2)			

(Note 1) The N.C pin does not have internal connection. Open the pin when mounting board. (Note 2) The EXP-Pad pin is connected to GND on the mounting board.

Block Diagram



Description of Blocks

1 INTERNAL REGULATOR

This is regulator block for internal circuits. This block shuts itself down at the shutdown status of SDX/EN pin voltage V_{SDX} or less. When SDX/EN pin voltage rises above V_{SDX}, IC consumption current increases. When SDX/EN pin voltage is above V_{EN1}, IC enters the enable status and starts switching operation. The soft start function operates for t_{SS} period from switching start, and the output voltage rises slowly. When SDX/EN pin voltage falls below V_{EN2}, IC enters the disable status and the switching operation is stopped.



Figure 1. Startup and Stop Timing Chart

2 Input Low Voltage Lock Out (UVLO)

This is the protection function for the low input voltage of the VIN pin.

When VIN pin voltage falls below V_{UVLO1}, IC detects UVLO and stops switching operation.

When VIN pin voltage rises above V_{UVLO2} , IC starts switching operation and a soft start function operates during the period of tss.



Figure 2. VIN UVLO Timing Chart

Description of Blocks – continued

3 Thermal Shutdown (TSD)

This block is the thermal shutdown circuit that prevents heat damage to the IC. When IC junction temperature rises more than 175 °C (Typ), IC stops switching operation. After that, when IC junction temperature falls IC restarts. The temperature hysteresis is 25 °C (Typ). The TSD function aims to protect itself. So IC junction temperature should be designed less than Tjmax = 150 °C. For that, it should not use as over temperature protection function of application.

4 SW VOLTAGE DETECTION

This block detects the flyback voltage generated in the SW pin. In turn-off of the transformer, this block converts current to flow from the FB pin into voltage by the resistance of the REF pin and the flyback voltage is detected by this REF pin voltage.

The IC controls REF pin voltage to be equivalent to VINTREF.

5 SOFT START

When IC turns to enable status that SDX/EN pin voltage rises above V_{EN1} , the comparison voltage of the PWM COMPARATOR block increases gradually from 0 V to V_{INTREF} . PWM comparator voltage is constantly V_{INTREF} after soft start time passed.

This operation prevents from the output voltage overshooting. The soft start time is fixed to t_{SS} in the IC. And, SCP protection is invalid for $t_{MASKSCP}$ period from start-up.

6 PWM COMPARATOR

This block compares REF pin voltage equivalent to feedback voltage of the output voltage with soft start voltage or reference voltage V_{INTREF}. This comparator output decides the ON timing. Since it does not have error amplifier and constitutes a feedback loop by the comparator, IC enables fast control to load response during PWM operation.

7 ADAPTIVE ON TIME CONTROLLER

This block is ON time control block which uses original adapted ON-time control technology.

Stable load current:	IC operates in PWM operation by constant ON time control.
Fluctuating load current:	IC operates in the constant ON time control and fluctuate the switching
	frequency. It results from fast response.
Light load:	The switching frequency decreases and realizes a high efficiency by PFM
	operation during discontinuous mode.

When the load current fluctuates, IC operates within f_{SW_MAX} . IC raises the primary average current by shortening the off time. It results from increasing the secondary current and secondary output voltage is quickly stable.





8 Maximum Frequency Limit Function (MAX FREQ)

This function limits the maximum frequency. The switching frequency is instantly high at ON width control in start-up or load response. It may influence to EMI. For that, IC limits max frequency less than f_{SW_MAX}.

9 DRIVER

This is the block which drives Nch MOSFET for switching.

10 Nch MOSFET

This is Nch MOSFET for switching.

Description of Blocks – continued

11 LOAD COMPENSATION

This block compensates the decrease of output voltage caused by the change of V_F characteristic in the secondary output diode which is proportional to load current. It monitors the current flown to the switching MOSFET and a part of the current flows to the REF pin. The quantity of compensation determines by the external resistor and capacitor at the L_COMP pin and K_{L_COMP} which is coefficient for SW current. For that, as the current flown from the FB pin to the external resistor of the REF pin decreases, the output voltage decrease is compensated.

12 Frequency Spectrum Spread (SPECTRUM SPREAD)

This is the function to spread switching frequency. The frequency spreading in the range of ± 5 % contributes to low EMI.

13 Over Current Protection (OCP), Battery Short Protection (BSP)

This function is over current protection of the MOSFET.

13.1 Over Current Protection (OCP)

When the switching MOSFET is on, as the primary transformer peak current becomes ILIMIT or more, IC detects the over current and the switching MOSFET is turned off. Because IC detects OCP per switching cycles, ON duty is limited and the output voltage drops. In addition, to prevent miss detection by turn ON surge, the detection of OCP is invalid for toN_MIN after the switching MOSFET is turned on.

After IC detects OCP, switching MOSFET is turn off after a delay time. When VIN voltage is increased, I_{LIMIT} is higher by the rise of current slope. ΔI_{LIMIT} depends on L_P value of transformer.

$$\Delta I_{LIMIT} = VIN \times t_{DELAY} / L_P$$

 t_{DELAY} : OCP detection delay time

 L_P : Primary inductance

 t_{DELAY} is always 0.2 µs or less.



13.2 Battery Short Protection (BSP)

In the case of increasing peak current by CCM (Continuous Conduction Mode) operation such as the short of the transformer winding or output short of secondary, large current over I_{LIMIT} is flown to the switching MOSFET. To prevent this phenomenon, IC is built-in BSP function. When SW pin current becomes I_{BSP} or more at the switching MOSFET ON, the IC detects BSP. By this function, the switching operation is stopped in the period of t_{BSP}. After it passes t_{BSP}, IC recovers switching operation without soft-start function. When BSP state continues, IC stops switching operation by SCP protection because output voltage is low. BSP is affected by the delay time (t_{DELAY}) the same as OCP, and I_{BSP} increases according to VIN voltage. Also, when primary transformer is short, the function is operated.



Description of Blocks – continued

14 Short Circuit Protection (SCP), REF Pin Open Protection (REFOPEN)

This is the block of the short protection and the open protection of the REF pin.

14.1 Short Circuit Protection (SCP)

As IC converts the primary flyback voltage to REF pin voltage, IC detects secondary output status. When secondary output voltage drops, REF pin voltage also drops. When REF pin voltage is below V_{SCP}, IC detects SCP. When the detection continues for t_{MASK}, the switching operation is stopped. After the time of t_{RESTART} passes from the stop, IC restarts with soft start function. To prevent SCP miss detection, the detection of SCP is invalid for t_{MASKSCP} at start-up. When REF voltage is lower than V_{SCP} for t_{MASKSCP} from start-up, IC stops switching for t_{RESTART}.





14.2 REF Pin Open Protection (REFOPEN)

The REF pin detects the secondary output voltage status from the primary flyback voltage. When the REF pin is open, output status is not detected, and switching MOSFET may occur malfunction. Therefore, when REF pin voltage is above V_{REFOP} , the IC detects REFOPEN protection. When the detection continues for t_{MASK} , the switching operation is stopped. After the time of $t_{RESTART}$ from the stop, IC restarts with soft start function. When auto recovery, IC operates for t_{MASK} from start-up. When REF pin voltage is above V_{REFOP} for t_{MASK} , IC stops switching for $t_{RESTART}$.





Absolute Maximum Ratings (Ta = 25 °C)

Parameter	Symbol	Rating	Unit
VIN Pin Voltage	V _{IN}	-0.3 to +45	V
SW Pin Voltage	Vsw	-0.3 to +62	V
SDX/EN Pin Voltage	V _{SDX/EN}	-0.3 to +45	V
FB Pin Voltage	Vfb	-0.3 to +45	V
REF Pin Voltage	VREF	-0.3 to +7	V
L_COMP Pin Voltage	VL_COMP	-0.3 to +7	V
Maximum Junction Temperature	Tjmax	150	°C
Storage Temperature Range	Tstg	-55 to +150	°C

Caution 1: Operating the IC over the absolute maximum ratings may damage the IC. The damage can either be a short circuit between pins or an open circuit between pins and the internal circuitry. Therefore, it is important to consider circuit protection measures, such as adding a fuse, in case the IC is operated over the absolute maximum ratings.

Caution 2: Should by any chance the maximum junction temperature rating be exceeded the rise in temperature of the chip may result in deterioration of the properties of the chip. In case of exceeding this absolute maximum rating, design a PCB with thermal resistance taken into consideration by increasing board size and copper area so as not to exceed the maximum junction temperature rating.

Thermal Resistance(Note 1)

Parameter	Symbol	Thermal Res	Linit	
Parameter	Symbol	1s ^(Note 3)	2s2p ^(Note 4)	Unit
HTSOP-J8	<u> </u>			
Junction to Ambient	θ _{JA}	206.4	45.2	°C/W
Junction to Top Characterization Parameter ^(Note 2)	Ψ_{JT}	21	13	°C/W

(Note 1) Based on JESD51-2 A (Still-Air).

(Note 2) The thermal characterization parameter to report the difference between junction temperature and the temperature at the top center of the outside surface of the component package.

(Note 3) Using a PCB board based on JESD51-3. (Note 4) Using a PCB board based on JESD51-5. 7

(Note 4) Using a PCB board based on JESD51-5, 7.							
Layer Number of Measurement Board	Material	Board Size					
Single	FR-4	114.3 mm x 76.2 mm x	114.3 mm x 76.2 mm x 1.57 mmt				
Тор							
Copper Pattern	Thickness						
Footprints and Traces	70 µm						
Layer Number of	Material	Board Size Thermal Via ^(Note 5)			te 5)		
Measurement Board	Material	Board Size		Pitch	Γ	Diameter	
4 Layers	FR-4	114.3 mm x 76.2 mm	x 1.6 mmt	1.20 mm Φ0		0.30 mm	
Тор		2 Internal Layers		Botte	om		
Copper Pattern	Thickness	Copper Pattern Thickness		Copper Pattern		Thickness	
Footprints and Traces	70 µm	74.2 mm x 74.2 mm 35 µm		74.2 mm x 74.2 mm		70 µm	
(Mate C) This the sum all via as we act with							

(Note 5) This thermal via connect with the copper pattern of layers 1,2, and 4. The placement and dimensions obey a land pattern.

Recommended Operating Conditions

Parameter	Symbol	Min	Тур	Max	Unit	Conditions
Operation Power Supply Voltage Range	VIN	3.4	12.0	42.0	V	VIN pin voltage
Operation Voltage Range	V _{SW}	-	-	60	V	SW pin Voltage
Operation Temperature	Topr	-40	-	+125	°C	
REF Pin Resistor	RREF	-	2.7	-	kΩ	External resistor value ^(Note 6)
L_COMP Voltage Range	VL_COMP	-	-	1.00	V	L_COMP pin voltage
VIN-GND Capacitor	CVIN	10	-	-	μF	

(Note 6) Set the REF resistor value of 2.7 kΩ (Typ). Choose the resistance accuracy for an output voltage accuracy.

Electrical Characteristics (Unless otherwise Ti = -40 °C to +150 °C. VIN = 12 V. VSDX/FN = 2.5 V)

Parameter	Symbol	Min	Тур	Max	Unit	Conditions
Power Supply Block						
Current at Shutdown	Ist	-	0	10	μA	SDX/EN = 0.3 V Tj ≤ 125 °C
Operating Current at No Switching	Icc	0.43	1.00	1.70	mA	REF = 0.6 V
UVLO Detection Voltage 1	VUVL01	3.00	3.20	3.40	V	At the VIN pin falling
UVLO Detection Voltage 2	VUVLO2	3.20	3.40	3.60	V	At the VIN pin rising
UVLO Voltage Hysteresis	VUVLO_HYS	0.12	0.20	0.28	V	
Shutdown and Enable Control Block						
Shutdown Voltage at the SDX/EN Pin	V _{SDX}	-	-	0.3	V	
Enable Voltage 1	V _{EN1}	1.90	2.00	2.10	V	At the SDX/EN pin rising
Enable Voltage 2	V _{EN2}	1.60	1.80	2.00	V	At the SDX/EN pin falling
Enable Voltage Hysteresis	VEN_HYS	0.14	0.20	0.26	V	
SDX/EN Pin Current	ISDX/EN	0.50	1.00	2.00	μA	SDX/EN = 2.5 V
SDX/EN Pin Pull-down Resistance	R _{SDX/EN}	1250	2500	3750	kΩ	
Reference Voltage Block						
Reference Voltage	VINTREF	0.525	0.540	0.555	V	
REF Pin Current	IREF	140	200	260	μA	R _{REF} = 2.7 kΩ
Switching Block						
On Resistance	Ron	-	0.40	0.80	Ω	SW-GND I _{SW} = 50 mA
Over Current Detection Current	I _{LIMIT}	2.08	2.60	3.12	Α	
BSP Detection Current	IBSP	2.39	3.38	4.52	Α	
Averaging Switching Frequency	f _{SW}	300	363	430	kHz	At PWM operation (Duty = 40 %)
Maximum Switching Frequency	f _{SW_MAX}	-	-	498	kHz	
On Time	t _{ON}	0.962	1.102	1.270	μs	At PWM operation (Duty = 40 %)
Minimum ON Time	ton_min	120	250	380	ns	
Maximum OFF Time	toff_max	25	35	45	μs	
Soft Start Time	tss	3.0	5.0	7.0	ms	From switching start to V _{INTREI} x 90 %
Protection Function Block						
Short Protection Detection Voltage	VSCP	0.20	0.30	0.40	V	
REFOPEN Protection Detection Voltage	VREFOP	0.60	0.70	0.80	V	
SCP/REFOPEN Detection Mask Time	t MASK	1.05	1.50	1.95	ms	
SCP Mask Time at Start-up	t MASKSCP	5.25	7.50	9.75	ms	
BSP Stop Time at Detection	t _{BSP}	262	375	488	μs	
Restart Time	t RESTART	18.0	24.0	30.0	ms	
Load Compensation Block						
KL_COMP (Compensation Coefficient of REF Current for SW Current)	K _{L_COMP}	0.090	0.128	0.166	%/MΩ	(Note 1)

(Note 1) Load compensation current coefficient is the coefficient which compensates output voltage decrease for output current. It sets by L_COMP pin resistor. It is tested at R_{L_COMP} = 10 kΩ.



Figure 8. Current at Shutdown vs Temperature



Figure 10. UVLO Detection Voltage1 vs Temperature



Figure 9. Operating Current at No Switching vs Temperature



Figure 11. UVLO Detection Voltage2 vs Temperature

(Reference Data)



Figure 12. UVLO Voltage Hysteresis vs Temperature



Figure 14. Enable Voltage1 vs Temperature



Figure 13. Shutdown Voltage at the SDX/EN Pin vs Temperature



Figure 15. Enable Voltage2 vs Temperature

Datasheet



Figure 16. Enable Voltage Hysteresis vs Temperature



Figure 18. SDX/EN Pin Pull-down Resistance vs Temperature



Figure 17. SDX/EN Pin Current vs Temperature



Figure 19. Reference Voltage vs Temperature



Figure 20. REF Pin Current vs Temperature



Figure 22. Over Current Detection Current vs Temperature



Figure 21. On Resistance vs Temperature



Figure 23. BSP Detection Current vs Temperature



Figure 24. Averaging Switching Frequency vs Temperature



Figure 26. On Time vs Temperature (Duty = 40 %, f_{SW} = 363 kHz)



Figure 25. Maximum Switching Frequency vs Temperature



Figure 27. Minimum ON Time vs Temperature



Figure 28. Maximum OFF Time vs Temperature



Figure 30. Short Protection Detection Voltage vs Temperature



Figure 29. Soft Start Time vs Temperature



Figure 31. REFOPEN Protection Detection Voltage vs Temperature



Figure 32. SCP/REFOPEN Detection Mask Time vs Temperature



Figure 34. BSP Stop Time vs Temperature



Figure 33. SCP Mask Time at Start-up vs Temperature



Figure 35. Restart Time vs Temperature



Figure 36. KL_COMP vs Temperature

Application Examples

1 Output Voltage

When the internal switching MOSFET is off, SW pin voltage "V_{SW}" is higher than VIN pin voltage. The secondary output voltage is calculated by the primary flyback voltage, which is described by the difference between this SW pin voltage and VIN pin voltage. SW pin voltage at turn off is calculated by the following formula.

$$V_{SW} = V_{IN} + \frac{N_P}{N_S} \times (V_{OUT} + V_F)$$
[V]

where:

 V_{SW} is SW pin voltage.

 V_{IN} is VIN pin voltage.

 N_P is the number of winding at the primary transformer.

 $N_{
m S}\,$ is the number of winding at the secondary transformer.

 V_{OUT} is the Output voltage.

 V_F is the forward voltage of the secondary output diode.



Figure 37. Application Block Diagram

The external resistor R_{FB} between the FB pin and the SW pin converts the primary flyback voltage into FB pin inflow current I_{FB} . I_{FB} is calculated by the formula below because FB pin voltage is nearly equal to VIN pin voltage by IC's internal circuit.

$$I_{FB} = \frac{V_{SW} - V_{FB}}{R_{FB}} = \frac{V_{IN} + \frac{N_P}{N_S} \times (V_{OUT} + V_F) - V_{FB}}{R_{FB}} = \frac{\frac{N_P}{N_S} \times (V_{OUT} + V_F)}{R_{FB}}$$
[A]

where:

 I_{FB} is FB pin inflow current.

 V_{FB} is FB pin voltage.

 $R_{FB}\,$ is the external resistor between the FB pin and the SW pin.

1 Output Voltage – continued

FB current I_{RFB} flows to the REF pin and the external resistor R_{REF} between the REF pin and the GND pin. REF pin voltage is calculated by below equation.

$$V_{REF} = \frac{R_{REF}}{R_{FB}} \times \frac{N_P}{N_S} \times (V_{OUT} + V_F)$$
[V]

where:

 V_{REF} is REF pin voltage.

 R_{REF} is the external resistor between the REF pin and the GND pin.

 R_{REF} resistor is necessary to set 2.7 k Ω because REF pin current is equivalent to I_{REF} and REF pin voltage is equivalent to V_{INTREF} .

$$R_{REF} = \frac{0.54 \, V}{200 \, \mu A} = 2 .7 \, k\Omega$$

Therefore, REF pin resistor is always needed to set R_{REF} = 2.7 k Ω .

REF pin voltage is input to the comparator with the reference voltage V_{INTREF} in the IC. By the internal circuit, REF pin voltage is equal to the reference voltage. Therefore, the output voltage and REF pin voltage is calculated by the formula below.

$$V_{OUT} = \frac{R_{FB}}{R_{REF}} \times \frac{N_S}{N_P} \times V_{INTREF} - V_F$$
[V]

To be shown to the equation, the output voltage is set by the number of winding ratio of the primary and secondary transformer (N_P/N_S) and the resistance ratio of R_{FB} and R_{REF} . According to the relational expression in above, the external resistor R_{FB} between the FB pin and the SW pin is calculated by the formula below.

$$R_{FB} = \frac{R_{REF}}{V_{INTREF}} \times \frac{N_P}{N_S} \times (V_{OUT} + V_F)$$
 [\Omega]

The ESR of the transformer on the secondary side as well as V_F causes the output voltage drop.

And, when transformer coupling is low, the N_P/N_S turns ratio changes and output voltage is lower than the setting voltage. Therefore, adjust the output voltage by actual evaluation of power supply.

2 Transformer

2.1 The Determine of Winding Ratio N_{P} / N_{S}

The winding ratio is the parameter for setting output voltage, Max output power, Duty, SW pin voltage. The duty of flyback converter is calculated by the following equation:

$$Duty = \frac{\frac{N_P}{N_S} \times (V_{OUT} + V_F)}{V_{IN} + \frac{N_P}{N_S} \times (V_{OUT} + V_F)}$$
[%]

 N_P is the Primary transformer winding

 N_S is the Secondary transformer winding

 V_{OUT} is the Output voltage

 V_F is the forward voltage of secondary output diode

 V_{IN} is VIN pin voltage

The winding ratio is calculated by below equation.

$$\frac{N_P}{N_S} = \frac{D_{TYP}}{1 - D_{TYP}} \times \frac{V_{IN}}{V_{OUT} + V_F}$$
$$D_{TYP} \text{ is the Duty of VIN voltage (Typ)}$$

In the middle VIN voltage of usual operating range, it recommends that D_{TYP} is set from 30 % to 50 %. First, it recommends to set D_{TYP} = 40 %. The winding ratio is limited by the maximum duty(D_{MAX}) in minimum input voltage condition. D_{MAX} given by the formula below must be not over 70 %. When duty is over 70 %, change D_{TYP} to be lower. If Duty is over 70 %, OFF time is short and the output voltage may change due to the shift in flyback voltage detection.

$$\frac{N_P}{N_S} = \frac{D_{MAX}}{1 - D_{MAX}} \times \frac{V_{IN(Min)}}{V_{OUT(Max)} + V_{F(Max)}}$$
where:

 D_{MAX} is the Maximum duty of minimum VIN voltage condition

 $V_{OUT(Max)}$ is the Maximum output voltage

 $V_{F(Max)}$ is the Maximum forward voltage (V_F) of Secondary diode

Flyback voltage is calculated by below calculation.

$$V_{OR} = (V_{OUT} + V_F) \times \frac{N_P}{N_s}$$
[V]

SW pin voltage calculated below must be set so that the withstand voltage is not exceeded.

$$V_{SW} = V_{IN(Max)} + V_{OR} + V_{SURGE}$$
 [V]

For example, when it has the delating of 90 % for SW pin voltage, SW pin voltage is needed to be less than the value which calculated below.

$$V_{SW} = 60 V \times (100 \% - 10 \%) = 54 V$$

In the case of $V_{IN(Max)}=30$ V and $V_{OR}=10$ V, V_{SURGE} voltage is needed to be less than 14 V. This value is calculated below.

$$54 V - (30 V + 10 V) = 14 V$$

V_{SURGE} is occurred by the leakage of transformer. If V_{SURGE} is higher, it needs to decrease the voltage by re-designing transformation structure or snubber circuit adjustment.



When designed transformer, temporarily set winding ratio to satisfy above. When the winding ratio is decided, R_{FB} can be set and V_{OUT} also can be set.

2 Transformer – continued

2.2 The Calculation of LP, Ls

The transformer should be set L_P and L_S value that power supply works CCM operation. For that, L_P and Ls is determined to use "k" which is the indicator of CCM operation. k is expressed from Figure 39 I_{SPK}, I_{SB} by the following equation.

$$k = (I_{SPK} - I_{SB})/I_{SPK}$$

where:

 I_{SPK} is the Secondary transformer peak current

 I_{SB} is the Secondary transformer bottom current

k is the Indicator of CCM ratio (It guides that it sets k = 0.25 when designing at first.)



Figure 39. The Waveform Example of Primary and Secondary Current of Transformer

where:

 I_{PPK} is the Primary transformer peak current

 I_{PB} is the Primary transformer bottom current

 I_{LIMIT} shown in electric characteristics determines maximum primary peak current. It enables to decide capable secondary minimum peak current from minimum I_{LIMIT} .

$$I_{SPK1(Min)} = I_{LIMIT(Min)} \times \frac{N_P}{N_c}$$
 [A]

Next, ISPK2(Max) is calculated from secondary maximum output current (IOUT(Max)).

$$I_{SPK2(Max)} = \frac{2 \times I_{OUT(Max)}}{(1 - D_{MAX}) \times (2 - k)} \times \frac{1}{\eta}$$
 [A]

 η is the Efficiency of power supply, it recommends to set to about 70 %

In order to output $I_{OUT(Max)}$, the condition of $I_{SPK2(Max)} < I_{SPK1(Min)}$ must be satisfied.

If not satisfied, re-design to change k value. The higher the k value, the wider the load area of DCM (Discontinuous Conduction Mode) operation. k = 1 means that the operation is DCM at all loads. IC has advantage of fast response and low EMI characteristics in CCM operation. For that, k is recommended lower value. Even if k value is high, there is no problem to output voltage regulation operation.

The secondary inductance $L_{S(Max)}$ is calculated by the following equation.

$$L_{S(Max)} = \frac{(2-k) \times (V_{OUT} + V_F) \times (1 - D_{MAX})^2}{2 \times I_{OUT(Max)} \times f_{sw(Max)} \times k}$$
[µH]

where:

 $f_{SW(Max)}$ is the Switching frequency (f_{SW(Max)} is set to 430 kHz in IC)

 $I_{OUT(Max)}$ is the Maximum secondary output current

Primary inductance L_P is calculated by below.

$$L_P = L_S \times (\frac{N_P}{N_S})^2 \qquad [\mu H]$$

2 Transformer – continued

2.3 The Calculation of IPRMS and ISRMS

Maximum primary RMS current (IPRMS) and Maximum secondary RMS current (ISRMS) are calculated below.

$$I_{PRMS} = \sqrt{\frac{(I_{PPK}^{2} + I_{PPK} \times I_{PB} + I_{PB}^{2}) \times D_{MAX}}{3}}$$
[A]
$$I_{SRMS} = \sqrt{\frac{(I_{SPK}^{2} + I_{SPK} \times I_{SB} + I_{SB}^{2}) \times (1 - D_{MAX})}{3}}$$
[A]

When selecting the wire diameter of transformer, refer to this RMS current.

3 **Output Capacitor**

The output capacitor place as close to the secondary diode as possible. Output capacitor value COUT is needed to set from the output ripple voltage (ΔV_0) and start-up time. The output ripple voltage which occurs by switching is calculated by below equation.

$$\Delta V_O = \frac{I_{OUT(Max)} \times D_{MAX}}{f_{SW(Max)} \times C_{OUT}}$$
[V]

On the other hand, when output capacitor is large, start-up time is long. When SCP detection mask time (tmaskscp) in start-up is passed, if REF voltage is lower than V_{SCP}, power supply cannot output. Therefore, COUT must be satisfied below condition.

$$C_{OUT} \leq \frac{1}{2} \times \frac{t_{MASKSCP(Min)} \times \{ \left(I_{LIMIT(Min)} \times \frac{N_P}{N_S} \right) \times (1 - Duty) - I_{OUT(Max)} \}}{V_{OUT} \times \left(\frac{V_{SCP(Max)}}{V_{INTREF(Min)}} \right)}$$
[µF]
Here, $\frac{V_{SCP(Max)}}{V_{SCP(Max)}} = 0.762$

ere,
$$\frac{V_{SCP(Max)}}{V_{INTREF(Min)}} = 0.7$$

A large output capacitance is required to hold the output voltage for load response or input voltage response. As a guide for output capacitor, it recommends the capacitance of 20 µF or more. And, ceramic capacitor may be lower capacitance because of temperature characteristics and variance, DC bias characteristics. It needs to select the parts to care them.

Input Capacitor 4

It uses ceramic capacitor to input capacitor and it is placed as close to the IC as possible. The capacitor value is set 10 µF or more.

5 Secondary Output Diode

Because the forward voltage (V_F) of secondary output diode causes an error in the output voltage, it needs to use SBD or FRD which is low forward voltage (V_F). And, the peak of diode reverse voltage must not exceed the rating of the diode. The secondary RMS current must be set that it does not exceed the rating current. Generally, it is recommended that the reverse voltage of secondary output diode sets to have margin of 30 % or more.

$$V_R = (V_{IN(Max)} \times \frac{N_S}{N_P} + V_{OUT}) \times 1.3 + V_{SURGE}$$
[V]

where:

 V_R is the reverse voltage of secondary output diode

 $V_{IN(Max)}$ is VIN maximum pin voltage

 N_P is the primary winding turns of transformer

 N_S is the secondary winding turns of transformer

 V_{OUT} is the Output voltage

 V_{SURGE} is the Surge voltage of transformer generated to the diode

And it is recommended that rating current of output diode margin twice or more for I_{SRMS}.

6 Output Resistor and Output Zener Diode (Minimum Load Current)

The output voltage raises in no load or light load. This is the reason IC is always worked by the minimum switching frequency which is determined by maximum OFF time toFF_MAX and minimum ON time toN_MIN at light loads. Because power supply supplies minimum power POMIN by this minimum switching frequency, output voltage raises when secondary power is lighter than Po_MIN. Po_MIN is calculated by below.

$$P_{O_MIN} = \frac{V_{IN(Max)}^{2}}{2 \times L_{P}} \times t_{ON_MIN(Max)}^{2} \times \frac{1}{t_{ON_MIN(Max)} + t_{OFF_MAX(Min)}}$$
[W]
$$I_{OUT_MIN} = \frac{P_{O_MIN}}{V_{OUT}}$$
By the equation, I_{OUT_MIN} can be also calculated.

When the raise of secondary output voltage is unacceptable, it needs to connect zener diode to secondary output. It operates output voltage suppression less than zener diode voltage.

And it can prevent to rise output voltage by losses which is occurred to connect resistors to secondary output. The secondary load resistor R_{OUT} is less than below equation is needed. Secondary resistor loss is calculated by the equation.

$$P_{LOSS} = \frac{V_{OUT}^{2}}{R_{OUT}} \qquad [W]$$

$$R_{OUT} \leq \frac{V_{OUT}^{2}}{P_{O_MIN}} = \frac{V_{OIT}^{2}}{\frac{V_{IN(Max)}^{2}}{2 \times L_{P}} \times t_{ON_MIN(Max)}^{2} \times \frac{1}{t_{ON_MIN(Max)} + t_{OFF_MAX(Min)}} \qquad [\Omega]$$

In fact, even if R_{OUT} resistance which is calculated above equation is used, output voltage rises transiently in switching OFF time. For that, R_{OUT} should be set low enough. R_{OUT} needs to adjust through evaluation. R_{OUT} resistor is needed to notice power dissipation.

The reason of output voltage raise refers to Application Examples: "10.The Influence to Frequency and Output Voltage for Each Load".



Figure 40. Zener Diode and Resistor to Secondary Output

7 Snubber Circuit

When the combination degree of transformer is low or large current line of board is long, the large surge voltage may be occurred in the SW pin at turn OFF timing of MOSFET. Preventing it, the snubber circuit shown in figure 41 is used. This snubber circuit clamps fly-back voltage + surge voltage when the voltage exceeds snubber voltage.



The clamp voltage is determined the following equation.

$$V_{CLAMP} = V_{F2} + V_z \qquad [V]$$

where:

 V_{CLAMP} is the Clamp setting voltage of snubber circuit

 V_{F2} is the Forward voltage of SBD

 V_z is the Zener diode voltage

When the clamp setting voltage is lower than flyback voltage (equal to $\frac{N_P}{N_S} \times (V_{OUT} + V_F)$), large current flows to Zener diode in the turn off. Therefore, the snubber voltage (V_{CLAMP}) must be higher than flyback voltage. When snubber circuit is slow response, it may not clamp setting voltage. So, SW voltage must be evaluated.

8 Setting of SDX/EN Pin Resistor

8.1 Setting of Enable Voltage

It can set enable voltage V_{IN_ENABLE} by following equation after releasing VIN UVLO.

$$V_{IN_ENABLE} = V_{EN1} \times \frac{R_1 + (R_2 / / R_{SDX/EN})}{R_2 / / R_{SDX/EN}} \qquad [V]$$

where:

 $V_{IN ENABLE}$ is the Target VIN operating start voltage

 V_{EN1} is the Enable voltage 1

 $R_2//R_{SDX/EN}$ is the Divided resistor between R₂ and R_{SDX/EN} which is IC internal resistor



Figure 42. Resistors Connected to the SDX/EN Pin

8.2 Setting of Disable Voltage

It can set disable voltage $V_{IN_DISABLE}$ at VIN pin voltage falling by following equation.

$$V_{IN_DISABLE} = V_{EN2} \times \frac{R_1 + (R_2//R_{SDX/EN})}{R_2//R_{SDX/EN}}$$
 [V]

where:

 $V_{IN_{DISABLE}}$ is the Target VIN operating stop voltage V_{EN2} is the Enable voltage2

The Output Voltage Compensation Function by L COMP Pin Resistor 9

This IC is built in output voltage compensation function which is prevented that output voltage decrease when primary transformer peak current (IP) increase. The cause of the drop of output voltage VOUT are the forward voltage change of secondary diode and transformer leakage etc. The example of output voltage compensation is shown in Figure 43.



Figure 43. L_COMP Voltage Compensation Example

This function compensates the output voltage by increasing IREFCOMP current to the REF current that determines the output voltage.

$$V_{OUT} = R_{FB} \times \frac{N_S}{N_P} \times \left(\frac{V_{INTREF}}{R_{REF}} + I_{REFCOMP}\right) - V_F \quad [V]$$

/INTREF is fiexed to 200 μA (Typ). IREFCOMP is increased for primary current increasing. As the result, **REF** current R_{REF} output voltage is compensated by output current on the secondary side. IREFCOMP is calculated to below.

$$I_{REFCOMP} = R_{L_COMP} \times K_{L_COMP} \times I_{SW(Ave)}$$
[µA]

where:

 $R_{L,COMP}$ is the Resistor connected to the L COMP pin

 $I_{SW(Ave)}$ is the Averaging current flown to the SW pin

 $K_{L,COMP}$ is the Fixed value determined by IC

Averaging current I_{SW(Ave)} of the SW pin can be converted below.

$$I_{SW(Ave)} = I_{S(Ave)} \times \frac{N_S}{N_P} = I_{OUT} \times \frac{1}{\eta} \times \frac{N_S}{N_P}$$
[A]

where:

 η is the efficiency (It recommends 70 % in design. And adjust R_{L COMP} in application evaluation.)

Because I_{SW(Ave)} is proportional to I_{OUT} as shown in the above equation, it enables to compensate output voltage. The compensation degree can adjust by resistor value of the L_COMP pin. Because Isw is triangle wave current, connect the capacitor 0.1 µF or more at the L COMP pin to flatten it.

The resistor value of the L_COMP pin is calculated by the following equation.

$$R_{L_COMP} = \frac{I_{REFCOMP}}{I_{SW(Ave)}} \times \frac{1}{K_{L\ COMP}}$$
 [kΩ]

Be sure to evaluate the output voltage characteristics in the application and adjust L COMP resistance as necessary. And, if the function is no use, the L COMP pin is needed to connect to GND.

10 The Influence to Frequency and Output Voltage for Each Load

This IC enables high efficiency to be lower switching frequency in light load. In CCM operation, the switching frequency is fsw for a constant load. When the load is light, the operation is changed from CCM operation to DCM operation. Then, switching frequency is reduced from fsw. The output load lout_fsw1 is calculated below.

$$I_{OUT}f_{SW1} = \frac{1}{2} \times \frac{(V_{IN} \times Duty)^2}{L_P \times f_{SW} \times V_{OUT}} \times \eta$$
 [A]

where:

 $I_{OUT} f_{SW1}$ is the Switched output current from DCM to CCM

 f_{SW} is the Switching frequency

 V_{IN} is VIN pin voltage

 L_P is the Primary inductance

 V_{OUT} is the Output voltage

 η is the Efficiency

As the load is further lightened, the ON time and OFF time decreases. ON time is operated by t_{ON_MIN} . The load current operated by t_{ON_MIN} is below.

$$I_{OUT}f_{SW2} = \frac{1}{2} \times \frac{f_{SW} \times (V_{IN} \times t_{ON}MIN)^2}{L_P \times V_{OUT}} \times \eta$$
 [A]

where:

 $I_{OUT} f_{SW2}$ is the Load current operated by minimum ON time

 $t_{ON MIN}$ is the Minimum ON time

As the load is further lightened, the ON time is not shorter than the t_{ON_MIN} and the OFF time is longer. Because IC is determined maximum OFF time. $f_{SW\ MIN}$ is calculated to below.

$$f_{SW_MIN} = \frac{1}{t_{ON_MIN} + t_{OFF_MAX}}$$
 [kHz]

where:

 $f_{SW MIN}$ is the Minimum switching frequency

 $t_{\it OFF\ MAX}$ is the Maximum OFF time

Therefore, constant output power is generated by f_{SW_MIN} operation in no load or light load. For that, output voltage raises in no load or light load.

And the IC builds in frequency spectrum spread function for EMI improvement. For that, the switching frequency is changed within a constant rate. An output voltage ripple which is dependent on spectrum spread occurs by the function.



Figure 44. Switching Frequency

I/O Equivalence Circuits

1	GND	2	SDX/EN	3	L_COMP	4	REF	
	GND	SDX/EN GND						
5	FB	6	N.C.	7	SW	8	VIN	
F				SW GND				

Operational Notes

1. Reverse Connection of Power Supply

Connecting the power supply in reverse polarity can damage the IC. Take precautions against reverse polarity when connecting the power supply, such as mounting an external diode between the power supply and the IC's power supply pins.

2. Power Supply Lines

Design the PCB layout pattern to provide low impedance supply lines. Furthermore, connect a capacitor to ground at all power supply pins. Consider the effect of temperature and aging on the capacitance value when using electrolytic capacitors.

3. Ground Voltage

Ensure that no pins are at a voltage below that of the ground pin at any time, even during transient condition.

4. Ground Wiring Pattern

When using both small-signal and large-current ground traces, the two ground traces should be routed separately but connected to a single ground at the reference point of the application board to avoid fluctuations in the small-signal ground caused by large currents. Also ensure that the ground traces of external components do not cause variations on the ground voltage. The ground lines must be as short and thick as possible to reduce line impedance.

5. Recommended Operating Conditions

The function and operation of the IC are guaranteed within the range specified by the recommended operating conditions. The characteristic values are guaranteed only under the conditions of each item specified by the electrical characteristics.

6. Inrush Current

When power is first supplied to the IC, it is possible that the internal logic may be unstable and inrush current may flow instantaneously due to the internal powering sequence and delays, especially if the IC has more than one power supply. Therefore, give special consideration to power coupling capacitance, power wiring, width of ground wiring, and routing of connections.

7. Testing on Application Boards

When testing the IC on an application board, connecting a capacitor directly to a low-impedance output pin may subject the IC to stress. Always discharge capacitors completely after each process or step. The IC's power supply should always be turned off completely before connecting or removing it from the test setup during the inspection process. To prevent damage from static discharge, ground the IC during assembly and use similar precautions during transport and storage.

8. Inter-pin Short and Mounting Errors

Ensure that the direction and position are correct when mounting the IC on the PCB. Incorrect mounting may result in damaging the IC. Avoid nearby pins being shorted to each other especially to ground, power supply and output pin. Inter-pin shorts could be due to many reasons such as metal particles, water droplets (in very humid environment) and unintentional solder bridge deposited in between pins during assembly to name a few.

9. Unused Input Pins

Input pins of an IC are often connected to the gate of a MOS transistor. The gate has extremely high impedance and extremely low capacitance. If left unconnected, the electric field from the outside can easily charge it. The small charge acquired in this way is enough to produce a significant effect on the conduction through the transistor and cause unexpected operation of the IC. So unless otherwise specified, unused input pins should be connected to the power supply or ground line.

Operational Notes – continued

10. Regarding the Input Pin of the IC

This monolithic IC contains P+ isolation and P substrate layers between adjacent elements in order to keep them isolated. P-N junctions are formed at the intersection of the P layers with the N layers of other elements, creating a parasitic diode or transistor. For example (refer to figure below):

When GND > Pin A and GND > Pin B, the P-N junction operates as a parasitic diode. When GND > Pin B, the P-N junction operates as a parasitic transistor.

Parasitic diodes inevitably occur in the structure of the IC. The operation of parasitic diodes can result in mutual interference among circuits, operational faults, or physical damage. Therefore, conditions that cause these diodes to operate, such as applying a voltage lower than the GND voltage to an input pin (and thus to the P substrate) should be avoided.



Figure 45. Example of Monolithic IC Structure

11. Ceramic Capacitor

When using a ceramic capacitor, determine a capacitance value considering the change of capacitance with temperature and the decrease in nominal capacitance due to DC bias and others.

12. Thermal Shutdown Circuit (TSD)

This IC has a built-in thermal shutdown circuit that prevents heat damage to the IC. Normal operation should always be within the IC's maximum junction temperature rating. If however the rating is exceeded for a continued period, the junction temperature (Tj) will rise which will activate the TSD circuit that will turn OFF power output pins. When the Tj falls below the TSD threshold, the circuits are automatically restored to normal operation.

Note that the TSD circuit operates in a situation that exceeds the absolute maximum ratings and therefore, under no circumstances, should the TSD circuit be used in a set design or for any purpose other than protecting the IC from heat damage.

13. Over Current Protection Circuit (OCP)

This IC incorporates an integrated overcurrent protection circuit that is activated when the load is shorted. This protection circuit is effective in preventing damage due to sudden and unexpected incidents. However, the IC should not be used in applications characterized by continuous operation or transitioning of the protection circuit.

Ordering Information



Marking Diagram



Physical Dimension and Packing Information Package Name HTSOP-J8 4. 9 ± 0.1 (Max5. 25 include. BURR) (3. 2) $4^{\circ} + 6^{\circ}_{-4^{\circ}}$ 8 7 6 5 2 4) 0±0. $9\pm0.$ 65 ± 0.15 (2. 2 6. $05\pm 0.$ 3. i. 0. 1 2 3 4 0.545 1PIN MARK $0.\ 1\ 7\ {}^{+0.}_{-0.}\ 0\ 3$ S-OMAX -i7 050 08 $0 8 \pm 0$. 85±0. 0. $42 \stackrel{+0.}{_{-0.}} \stackrel{0.5}{_{04}} \oplus 0. 08 \mathbb{M}$ 1. 27 (UNIT:mm) \Box 0. 08 S 0. 0. PKG:HTSOP-J8 Drawing No. EX169-5002-2 < Tape and Reel Information > Таре Embossed carrier tape Quantity 2500pcs Direction of feed E2 The direction is the pin 1 of product is at the upper left when you hold reel on the left hand and you pull out the tape on the right hand 0 0 0 0 0 0 0 0 Ο 0 Ο 0 E2 TR E2 TR E2 TR E2 TR E2 TR E2 TR ΤL E1 ΤL E1 ΤL ΤL E1 ΤL E1 E1 E1 ΤL Direction of feed Pocket Quadrants Reel

Revision History

Date	Revision	Changes
01.Mar.2022	001	New Release

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